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Rapid estimation of rate constants using on-line SW-NIR and trilinear models

Sabina Bijlsma^a, D.J. Louwerse (Ad)^a, Willem Windig^b, Age K. Smilde^{a,*}

^a*Process Analysis and Chemometrics, Department of Chemical Engineering, University of Amsterdam, Nieuwe Achtergracht 166, NL-1018 WV Amsterdam, Netherlands*

^b*Imaging Research and Advanced Development, Eastman Kodak Company, Rochester, NY 14650-2132, USA*

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Abstract

In this paper, two algorithms are presented to estimate reaction rate constants from on-line short-wavelength near-infrared (SW-NIR) measurements. These can be applied in cases where the contribution of the different species in the mixture spectra is of exponentially decaying character. From a single two-dimensional dataset two two-way datasets are formed by splitting the original dataset such that there is a constant time lag between the two two-way datasets. Next, a trilinear structure is formed by stacking these two two-way datasets into a three-way array. In the first algorithm, based on the generalized rank annihilation method (GRAM), the trilinear structure is decomposed by solving a generalized eigenvalue problem (GEP). Because GRAM is sensitive to noise it leads to rough estimations of reaction rate constants. The second algorithm (LM-PAR) is an iterative algorithm, which consists of a combination of the Levenberg–Marquardt algorithm and alternating least squares steps of the parallel factor analysis (PARAFAC) model using the GRAM results as initial values. Simulations and an application to a real dataset showed that both algorithms can be applied to estimate reaction rate constants in case of extreme spectral overlap of different species involved in the reacting system. © 1998 Elsevier Science B.V. All rights reserved.

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1. Introduction

Kinetic approaches have been recognized as very important in analytical chemistry [1]. For example, in chemical industry reaction rate constants of a certain chemical process can be monitored to check if the process is in or out of control. Therefore, it is important that the estimations for the reaction rate constants

are available rapidly in order to control the considered chemical process.

Short-wavelength near-infrared (SW-NIR) spectroscopy can be used to monitor on-line continuous and batch processes. The use of long pathlengths in SW-NIR is necessary to compensate for the weak extinction coefficients. In addition, long pathlengths ensure that a spectrum is more representative of the bulk and a spectrum is not disturbed by absorption of thin layers on the wall of the cell. A big advantage of the use of SW-NIR over NIR and IR for example, is the possible use of fiber optics, which makes it possible to measure

*Corresponding author. Fax: +31-20-5256638; e-mail: asmilde@anal.chem.uva.nl

on-line while the instrument is located in another safe place, not close to the process. A very extensive explanation of (SW)-NIR has been given by Workman [2].

If spectra have been obtained during a certain time interval of a process and the kinetic equations are available, iterative curve resolution methods can be used to estimate reaction rate constants because these parameters can be incorporated as “unknowns” [3]. Sylvestre et al. [4] showed this basic idea of estimating an unknown parameter, in this case a reaction rate constant, using recorded spectra from a unimolecular irreversible reaction for a certain time course and iterative curve resolution. Mayes et al. [5] determined the reaction rate constants of the pseudo-first-order two-step epoxidation of 2,5-di-*tert*-butyl-1,4-benzoquinone from SW-NIR spectra of the reacting system and iterative curve resolution. Tam and Chau [6] performed a multivariate study of kinetic data for a two-step consecutive reaction using target factor analysis. There are also methods to estimate reaction rate constants which are not based on iterative curve resolution. González et al. [7] describe many of these methods. However, in the mentioned papers, not much attention is paid to the experimental errors and instrumental noise which contribute to the estimate of the reaction rate constants.

In a previous work [8], a procedure has been described to estimate reaction rate constants from on-line SW-NIR measurements in the case of an extreme spectral overlap using two different iterative curve resolution algorithms, called the “standard” and the “weighted” algorithm, respectively. Simulations showed that both algorithms can be applied in case of an extreme spectral overlap of species involved in the considered reaction. The procedure was also applied to the pseudo-first-order two-step epoxidation of 2,5-di-*tert*-butyl-1,4-benzoquinone. Quality assessment of the estimated reaction rate constants was performed to investigate experimental errors and instrumental noise. The results showed that good estimations are possible.

In the literature, there are a number of available algorithms, based on curve resolution, for estimating unknown parameters from the recorded spectra [8–12]. However, those algorithms always have an iterative character which is not very attractive to use because of the time consuming iterations. Moreover,

the speed of iterative algorithms is not known in advance. The choice of the starting values also plays a crucial role. For every specific case the speed of a chosen iterative algorithm will be different. Especially if such algorithms are used to estimate parameters for example from on-line batch processes in industry, these have to be fast. A non-iterative algorithm which has a known speed in advance would be very convenient in this case, which need not be very accurate because a rough estimate of the reaction rate constants is very often satisfactory. A fast non-iterative algorithm is presented in this paper for the cases where a fast rough estimate of parameters is desirable. An improved iterative algorithm is also presented if more accurate estimates of parameters are wanted.

Recently, Windig and Antalek [13,14] developed a modification of the generalized rank annihilation method (GRAM) [15,16] which they have called the direct exponential curve resolution algorithm (DECRA). GRAM can be used if two experimental datasets have a very special relation. Suppose that the dataset from the first experiment can be expressed as a product of the concentration matrix and the matrix of pure spectra, and the datamatrix of the second experiment can be expressed as a product of the concentration matrix, a diagonal matrix with scaling factors and the matrix of pure spectra, respectively. Hence, the matrix of the pure spectra and the concentration matrix of the two experiments only differ by certain scaling factors.

If the contribution of the species in the mixture spectra is of exponentially decaying character, a modified GRAM method separates the two-dimensional dataset from only one single experiment in two different two-way datasets with a constant time lag. Next, the two different sets are stacked to construct a trilinear structure. Finally, a generalized eigenvalue problem (GEP) [15] can be solved to decompose the trilinear structure. In GEP loadings of the second and third mode are estimated using two samples. From the decomposition, specific parameters can be estimated. Hence, in fact DECRA is the same as GRAM except that the dataset from one single experiment is used to build two datasets. Windig and Antalek [14] used pulsed gradient spin echo nuclear magnetic resonance (PGSE NMR) data to show the performance of their described method in practice. In this application the decay is a function of the self-diffusion

coefficient and PGSE NMR has been used to determine these coefficients. Hence, it is also possible to estimate reaction rate constants using GRAM, because kinetic equations also have an exponentially decaying character.

If the noise level of data is low, the described GRAM procedure will perform very well. If the noise level is moderate, an iterative algorithm is necessary, unless a rough estimate of parameters is satisfactory. The estimations of the parameters from the solution of a GEP can be used as a very good set of starting values for the iterative algorithm. A combination of the Levenberg–Marquardt algorithm and alternating least squares steps of the PARAFAC [17–19] model using the GRAM results as initial values can be used as an iterative method to estimate parameters, as will be shown in this paper.

In this paper, simulations based on a two-step consecutive reaction are used to show that both algorithms described can be applied to estimate reaction rate constants in case of extreme spectral overlap of different species involved in the reacting system. The performance of both algorithms is also tested on the pseudo-first-order two-step epoxidation of 2,5-di-*tert*-butyl-1,4-benzoquinone [5,8,20]. Quality assessment of the estimated reaction rate constants is performed using the jackknife method [21].

2. Theory

2.1. Notation

Boldface capital characters denote matrices, boldface lower case characters denote vectors, boldface underlined capital characters denote a three-way array, **1** denotes a vector with ones and the superscript “T” denotes a transpose. $\mathbf{A}^{(j)}$ is the matrix **A** after the *j*th iteration, \mathbf{a}_i is the *i*th column of **A** and $\mathbf{a}_i^{(j)}$ is the *i*th column of **A** after the *j*th iteration. In Appendix A, there is a convenient summary of the nomenclature of the most important scalars, vectors and matrices used in this paper.

2.2. The model

2.2.1. Shifting an exponentially decaying function

Let an array of exponentially decaying numbers, called array one, be equal to 162, 54, 18, 6, 2. Next,

<u>Array one</u>		<u>Array two</u>
162		
54	$\xleftrightarrow{R = 162/54}$	162
18	$\xleftrightarrow{R = 54/18}$	54
6	$\xleftrightarrow{R = 18/6}$	18
2	$\xleftrightarrow{R = 6/2}$	6
		2

$R = \text{ratio} = 3 = \text{constant}$

Fig. 1. An array with exponentially decaying numbers (array one), the corresponding shifted array (array two) and the ratio between two numbers listed in the same row.

suppose array one is shifted to a position which results into array two according to Fig. 1. In Fig. 1, the ratio, *R*, between two numbers listed in one row is the same from row to row. In this case the ratio equals three.

The following equation represents an exponentially decaying function describing the reaction kinetics of a first-order process:

$$C = e^{-k_1 t}, \quad (1)$$

where k_1 is a reaction rate constant and *C* is the concentration of a certain species at time *t*. If the exponent is shifted with a time shift *S* Eq. (1) can be written as

$$C_s = e^{-k_1(t+S)}, \quad (2)$$

where C_s is the “shifted concentration”. The ratio of Eqs. (1) and (2), called λ , is an indirect measure for k_1 as is shown in the following equation:

$$\begin{aligned} \lambda = \frac{C}{C_s} &= \frac{e^{-k_1 t}}{e^{-k_1(t+S)}} = e^{-k_1 t + k_1(t+S)} \\ &= e^{k_1 S} \Rightarrow k_1 = \frac{\ln(\lambda)}{S}. \end{aligned} \quad (3)$$

Hence, if an exponentially decaying function is time shifted, the reaction rate constant can be extracted from the ratio of the non-shifted and the shifted exponentially decaying function.

2.2.2. Curve resolution and the reaction model

Let the matrix **X** (*M* × *N*) be a collection of spectra taken during a certain time course with *M* equidistant

time points at N wavelengths of a reacting system if K species are involved. In curve resolution the matrix \mathbf{X} can be expressed as the following equation assuming the Lambert–Beer law [22]:

$$\mathbf{X} = \mathbf{F}\mathbf{D}^T + \mathbf{E}. \quad (4)$$

The matrices from Eq. (4) have the following properties:

1. Every row in \mathbf{X} denotes a spectrum recorded at a certain time.
2. \mathbf{F} ($M \times K$) is the matrix with concentration profiles.
3. Every column in \mathbf{F} denotes the concentration profile of a species in time.
4. \mathbf{D} ($N \times K$) is the matrix containing the pure spectra of the species.
5. Every column in \mathbf{D} represents the pure spectrum of a species.
6. \mathbf{E} ($M \times N$) is a matrix of errors (model errors, experimental errors and instrumental noise).

Suppose that the following first-order consecutive reaction is considered as the reaction model.

Step 1: $U \rightarrow V$, with reaction rate constant k_1 .

Step 2: $V \rightarrow W$, with reaction rate constant k_2 .

Eqs. (5)–(7) are the kinetic rate equations, describing the concentration profiles of species U , V and W , respectively, with initially only U present:

$$C_{U,i} = C_{U,0} e^{-k_1 t_i}, \quad (5)$$

$$C_{V,i} = \frac{k_1 C_{U,0}}{(k_2 - k_1)} (e^{-k_1 t_i} - e^{-k_2 t_i}), \quad (6)$$

$$C_{W,i} = C_{U,0} - C_{U,i} - C_{V,i}, \quad (7)$$

where $C_{U,i}$, $C_{V,i}$ and $C_{W,i}$ are the concentration of species U , V and W at time t_i , respectively; $C_{U,0}$ is the initial concentration of species U at time 0. Eqs. (5)–(7) are the columns of the \mathbf{F} matrix. Hence, every column of \mathbf{F} represents a kinetic rate equation.

A representation of the datamatrix \mathbf{X} from Eq. (4) is given in Fig. 2, where \mathbf{d}_U , \mathbf{d}_V and \mathbf{d}_W with dimensions ($N \times 1$) are the pure spectra of species U , V and W , respectively; \mathbf{f}_U , \mathbf{f}_V and \mathbf{f}_W with dimensions ($M \times 1$) are the concentration profiles of species U , V and W , respectively. The vector $(e^{-k_1 t_1} \dots e^{-k_1 t_M})^T$ is reduced to the shortened notation $e^{-k_1 \mathbf{t}}$ and $\mathbf{t} = (t_1 \dots t_M)^T$. The concentration profiles of a simulated situation are

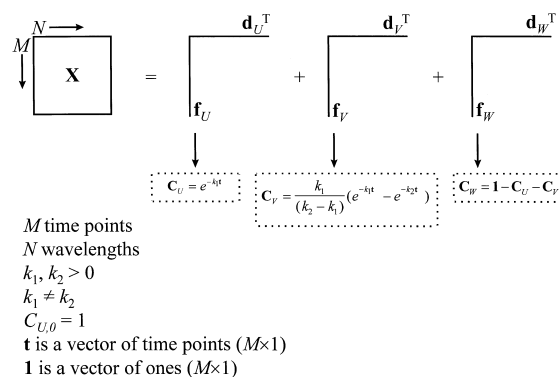


Fig. 2. Representation of the datamatrix \mathbf{X} if three species U , V and W are involved, where \mathbf{f}_U , \mathbf{f}_V and \mathbf{f}_W are the concentration profiles of species U , V and W , respectively; \mathbf{d}_U , \mathbf{d}_V and \mathbf{d}_W are the pure spectra of U , V and W , respectively; C_U , C_V and C_W are the concentration vectors of species U , V and W , respectively, and k_1 and k_2 are the reaction rate constants.

shown in Fig. 3, where $C_{U,0}$ equals 1, and k_1 and k_2 equal 0.30 min^{-1} and 0.05 min^{-1} , respectively.

2.2.3. The trilinear structure

Suppose for simplicity that only the first step of the reaction model described in Section 2.2.2 is considered. Hence, Eq. (5) is considered if only the concentration of the reactant is of interest and \mathbf{X} ($M \times N$) contains the SW-NIR measurements of only species U of reaction step 1. Next, \mathbf{X} will be used to build two matrices, $\mathbf{X}_1 = (\mathbf{X}([1 \dots (M-S)]) \times N)$ and $\mathbf{X}_2 = (\mathbf{X}([(1+S) \dots M]) \times N)$ by separating \mathbf{X} with a constant time shift S , which can be any positive integer value between 1 and $(M-1)$. The matrices formed by splitting \mathbf{X} according to Eq. (4) are visualized in Fig. 4, where \mathbf{d}_U ($N \times 1$) is the pure spectrum of species U , \mathbf{f}_U ($M \times 1$) is the concentration profile of species U , and \mathbf{f}_1 ($(M-S) \times 1$) and \mathbf{f}_2 ($(M-S) \times 1$) are the concentration profiles of species U with time shift S in matrices \mathbf{X}_1 and \mathbf{X}_2 , respectively.

The matrices \mathbf{X}_1 and \mathbf{X}_2 formed by splitting \mathbf{X} can be put into a trilinear or PARAFAC [17,18,19] model by means of stacking as shown in Fig. 5 to construct a three-way array $\underline{\mathbf{X}}$ ($(M-S) \times N \times 2$). The vector \mathbf{b} ($N \times 1$) is the pure spectrum of species U , \mathbf{a} ($(M-S) \times 1$) is the concentration profile of species U and \mathbf{c} (2×1) is the vector with scaling factors of \mathbf{X}_1 and \mathbf{X}_2 . From \mathbf{c} the reaction rate constant k_1 can be estimated if the time shift is known. An element x_{mnp}

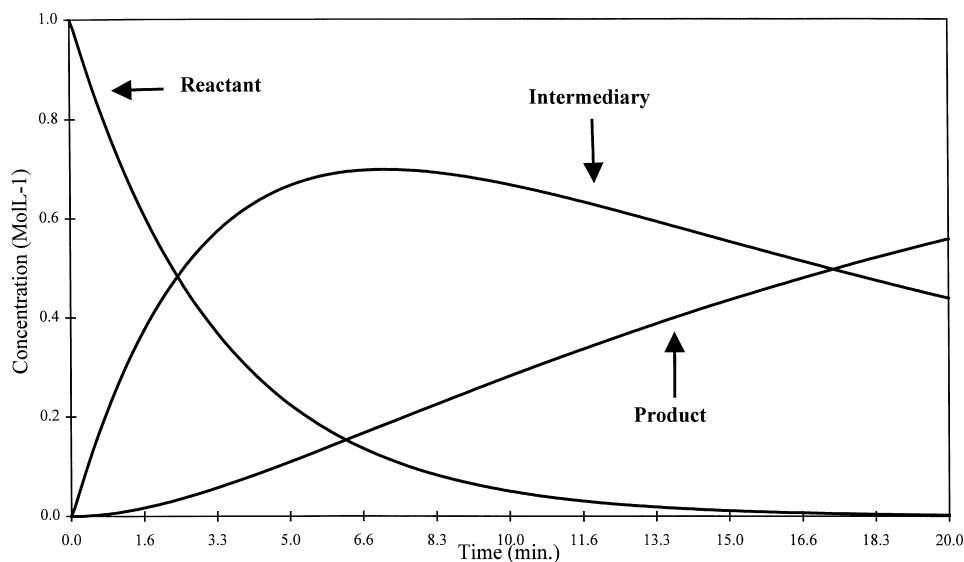


Fig. 3. The concentration profiles of three species (reactant, intermediary and product) for a simulated first order process as described in the text.

from \mathbf{X} with dimension $(M \times N \times P)$ is modeled by means of a one-factor PARAFAC model according to

$$x_{mnp} = a_{m1}b_{n1}c_{p1} + e_{mnp}. \quad (8)$$

If two exponentially decaying functions are considered, this will result in a two-component PARAFAC model. If more complex reaction schemes and therefore more exponentially decaying functions are considered, Eq. (8) can be generalized to a multi-

ple PARAFAC component model according to

$$x_{mnp} = \sum_{q=1}^Q a_{mq}b_{nq}c_{pq} + e_{mnp}. \quad (9)$$

Define the vectors \mathbf{a}_q , \mathbf{b}_q and \mathbf{c}_q as vectors with the elements a_{mq} , b_{nq} and c_{pq} , respectively. The multiplication of a_{mq} , b_{nq} and c_{pq} for each m, n, p gives the q th triad. Hence, every independent exponentially decaying function can be considered as a triad. The \mathbf{C} -matrix contains the scaling factors from which the different reaction rate constants can be estimated.

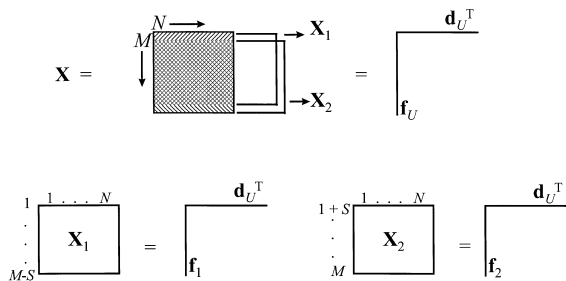


Fig. 4. Representation of datamatrix \mathbf{X} , \mathbf{X}_1 and \mathbf{X}_2 where \mathbf{X}_1 and \mathbf{X}_2 are formed by separating \mathbf{X} ; \mathbf{f}_U is the concentration profile of species U , \mathbf{d}_U is the pure spectrum of species U , \mathbf{f}_1 and \mathbf{f}_2 is both the concentration profiles for species U with a time shift, M is the number of time points, N is the number of wavelengths and S is the time shift.

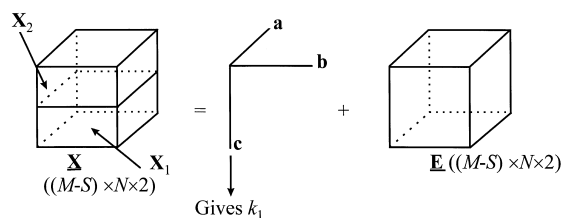


Fig. 5. The PARAFAC model: \mathbf{X} is the three-way array formed by stacking \mathbf{X}_1 and \mathbf{X}_2 ; \mathbf{E} is a three-way array with errors, \mathbf{a} is the concentration profile of species U , \mathbf{b} is the pure spectrum of species U , \mathbf{c} is the vector with scaling factors of \mathbf{X}_1 and \mathbf{X}_2 , M is the number of time points and N is the number of wavelengths.

Hence, every combination of exponentially decaying functions can be modeled, but every combination has to be written as a sum of separate exponentially decaying components.

Now, consider the two reactions from the reaction model described earlier in Section 2 and matrix \mathbf{X} ($M \times N$) with SW-NIR measurements of the reacting system. Suppose $C_{U,0}$ equals 1. Eqs. (5) and (6) are already a sum of exponentially decaying functions, but Eq. (7) is not decaying. Eq. (7) can be written, using Eqs. (5) and (6), as

$$C_{W,i} = 1 - e^{-k_1 t_i} - k(e^{-k_1 t_i} - e^{-k_2 t_i}) \\ = e^0 - e^{-k_1 t_i} - k e^{-k_1 t_i} + k e^{-k_2 t_i}, \quad (10)$$

where $k = k_1/(k_2 - k_1)$. Eq. (10) is now a sum of separate exponentially decaying functions. To make sure that the term e^0 is present in the dataset a column with constants ($M \times 1$), for example $(1 \dots 1)^T$, has to be added to the datamatrix \mathbf{X} ($M \times N$) to construct an augmented datamatrix \mathbf{X}^* ($M \times (N+1)$) [23,24]. The augmented datamatrix \mathbf{X}^* is visualized in Fig. 6, where \mathbf{s}_U , \mathbf{s}_V and \mathbf{s}_W with dimensions $((N+1) \times 1)$ are the pure spectra of species U , V and W , respectively; \mathbf{f}_U , \mathbf{f}_V and \mathbf{f}_W with dimensions $(M \times 1)$ are the concentration profiles of species U , V and W , respectively. The vector \mathbf{s}_L ($(N+1) \times 1$) is the “spectrum” of the added column with constants equal to: $(0 \ 0 \ 0 \ 0 \dots 0 \ 1)^T$. The vector \mathbf{f}_L ($M \times 1$) is the concentration profile of the added column with constants with

“concentration” C_L equal to e^0 . A mathematical representation of \mathbf{X}^* is given in the following equation:

$$\mathbf{X}^* = \mathbf{f}_U \mathbf{s}_U^T + \mathbf{f}_V \mathbf{s}_V^T + \mathbf{f}_W \mathbf{s}_W^T + \mathbf{f}_L \mathbf{s}_L^T. \quad (11)$$

Eq. (11) can be rewritten, after rewriting the vectors with the concentration profiles from Eq. (11) using Eqs. (5), (6) and (10) and the relation $k = k_1/(k_2 - k_1)$, as

$$\mathbf{X}^* = (e^{-k_1 \mathbf{t}}) \mathbf{s}_U^T + k(e^{-k_1 \mathbf{t}}) \mathbf{s}_V^T - k(e^{-k_2 \mathbf{t}}) \mathbf{s}_V^T \\ - (e^{-k_1 \mathbf{t}}) \mathbf{s}_W^T + e^{0\mathbf{t}} \mathbf{s}_W^T - k(e^{-k_1 \mathbf{t}}) \mathbf{s}_W^T + k(e^{-k_2 \mathbf{t}}) \mathbf{s}_W^T \\ + e^{0\mathbf{t}} \mathbf{s}_L^T = e^{-k_1 \mathbf{t}} (\mathbf{s}_U + k \mathbf{s}_V - \mathbf{s}_W - k \mathbf{s}_W)^T \\ + e^{-k_2 \mathbf{t}} (-k \mathbf{s}_V + k \mathbf{s}_W)^T + e^{0\mathbf{t}} (\mathbf{s}_W + \mathbf{s}_L)^T \\ = \mathbf{a}_1 \mathbf{b}_1 + \mathbf{a}_2 \mathbf{b}_2 + \mathbf{a}_3 \mathbf{b}_3, \quad (12)$$

where

$\mathbf{a}_1 = e^{-k_1 \mathbf{t}}$, $\mathbf{a}_2 = e^{-k_2 \mathbf{t}}$, $\mathbf{a}_3 = e^{0\mathbf{t}}$, $\mathbf{b}_1 = \mathbf{s}_U^T + k \mathbf{s}_V^T - \mathbf{s}_W^T - k \mathbf{s}_W^T$, $\mathbf{b}_2 = -k \mathbf{s}_V^T + k \mathbf{s}_W^T$ and $\mathbf{b}_3 = \mathbf{s}_W^T + \mathbf{s}_L^T$. Eq. (11) and the mathematical manipulation in Eq. (12) are visualized in Fig. 7. The concentration profiles, \mathbf{f}_U , \mathbf{f}_V and \mathbf{f}_W , are rearranged into the exponentially decaying functions \mathbf{a}_1 , \mathbf{a}_2 and \mathbf{a}_3 . The response matrix \mathbf{X}^* consists of a sum of exponentially decaying functions.

Next, \mathbf{X}^* will be used to build two datamatrices, \mathbf{X}_1^* and \mathbf{X}_2^* , using a time shift S . The matrices \mathbf{X}_1^* ($(M-S) \times (N+1)$) and \mathbf{X}_2^* ($(M-S) \times (N+1)$) formed by separating \mathbf{X}^* are used to construct the three-way array $\underline{\mathbf{X}}^*$ ($(M-S) \times (N+1) \times 2$) by stacking and can be modeled with PARAFAC as is shown in Fig. 8. From the three-way array $\underline{\mathbf{X}}^*$ the following three loading matrices can be constructed.

- $\mathbf{A} = [\mathbf{a}_1 \ \mathbf{a}_2 \ \mathbf{a}_3]$ ($(M-S) \times 3$) with k -rank [25] equal to 3.
- $\mathbf{B} = [\mathbf{b}_1 \ \mathbf{b}_2 \ \mathbf{b}_3]$ ($(N+1) \times 3$) with k -rank equal to 3.
- $\mathbf{C} = [\mathbf{c}_1 \ \mathbf{c}_2 \ \mathbf{c}_3]$ (2×3) with k -rank equal to 2, assuming $k_1 \neq k_2$.

The k -rank is defined as follows. Suppose a matrix has H columns. If any combination of L columns of the matrix is independent and this is not valid for $L+1$, then the k -rank of the matrix is equal to L . The three-way rank of $\underline{\mathbf{X}}^*$, called R , equals 3 in this case. For the decomposition of the three-way array in the matrices \mathbf{A} , \mathbf{B} and \mathbf{C} to be unique, the Kruskal criterion [26] has to be fulfilled. According to the Kruskal criterion, the decomposition is unique if the following equation is valid:

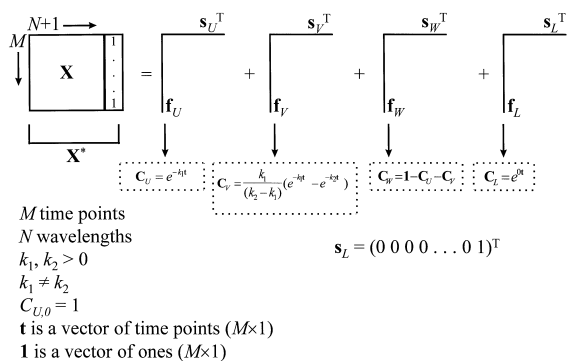


Fig. 6. Visualization of the augmented datamatrix \mathbf{X}^* , where \mathbf{s}_U , \mathbf{s}_V and \mathbf{s}_W are the pure spectra of species U , V and W , respectively; \mathbf{f}_U , \mathbf{f}_V and \mathbf{f}_W are the concentration profiles of species U , V and W , respectively. The vector \mathbf{s}_L is the “spectrum” of the added column with constants and \mathbf{f}_L is the concentration profile of the added column with constants.

$$\begin{aligned}
\mathbf{X}^* &= \begin{bmatrix} \mathbf{s}_U^T \\ \mathbf{f}_U \end{bmatrix} + \begin{bmatrix} \mathbf{s}_V^T \\ \mathbf{f}_V \end{bmatrix} + \begin{bmatrix} \mathbf{s}_W^T \\ \mathbf{f}_W \end{bmatrix} + \begin{bmatrix} \mathbf{s}_L^T \\ \mathbf{f}_L \end{bmatrix} = \begin{bmatrix} \mathbf{s}_U^T \\ e^{-k_1 t} \end{bmatrix} + \begin{bmatrix} \mathbf{s}_V^T \\ e^{-k_1 t} \end{bmatrix} + \\
&\begin{bmatrix} -k\mathbf{s}_V^T \\ e^{-k_2 t} \end{bmatrix} + \begin{bmatrix} -\mathbf{s}_W^T \\ e^{-k_1 t} \end{bmatrix} + \begin{bmatrix} \mathbf{s}_W^T \\ e^{0t} \end{bmatrix} + \begin{bmatrix} -k\mathbf{s}_W^T \\ e^{-k_1 t} \end{bmatrix} + \begin{bmatrix} k\mathbf{s}_W^T \\ e^{-k_2 t} \end{bmatrix} + \begin{bmatrix} \mathbf{s}_L^T \\ e^{0t} \end{bmatrix} = \\
&\begin{bmatrix} (\mathbf{s}_U^T + k\mathbf{s}_V^T - \mathbf{s}_W^T - k\mathbf{s}_W^T) \\ e^{-k_1 t} \end{bmatrix} + \begin{bmatrix} (-k\mathbf{s}_V^T + k\mathbf{s}_W^T) \\ e^{-k_2 t} \end{bmatrix} + \begin{bmatrix} (\mathbf{s}_W^T + \mathbf{s}_L^T) \\ e^{0t} \end{bmatrix} = \\
&\begin{bmatrix} \mathbf{b}_1 \\ \mathbf{a}_1 \end{bmatrix} + \begin{bmatrix} \mathbf{b}_2 \\ \mathbf{a}_2 \end{bmatrix} + \begin{bmatrix} \mathbf{b}_3 \\ \mathbf{a}_3 \end{bmatrix}
\end{aligned}$$

Fig. 7. Rewriting the augmented datamatrix \mathbf{X}^* from Fig. 6.

$$k\text{-rank}(\mathbf{A}) + k\text{-rank}(\mathbf{B}) + k\text{-rank}(\mathbf{C}) \geq 2R + 2. \quad (13)$$

In this case $(3+3+2) \geq (2 \times 3+2) \Rightarrow 8 \geq 8$ and hence the decomposition of the three-way array is unique.

2.3. The algorithms

A rough description of the most important steps of GRAM and LM-PAR can be found in Fig. 9.

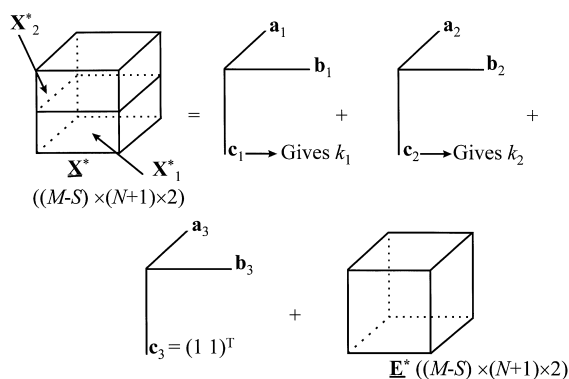


Fig. 8. The PARAFAC model: \mathbf{X}^* is formed by stacking \mathbf{X}_1^* and \mathbf{X}_2^* , \mathbf{E}^* is a matrix with errors, M is the number of time points, N is the number of wavelengths and k_1 and k_2 are the reaction rate constants. The vectors \mathbf{a}_1 , \mathbf{a}_2 , \mathbf{a}_3 , \mathbf{b}_1 , \mathbf{b}_2 and \mathbf{b}_3 are defined in the text just after Eq. (12).

2.3.1. Non-iterative algorithm: GRAM

In this section GRAM will be explained starting from the decomposition of the three-way array \mathbf{X}^* $((M-S) \times (N+1) \times 2)$.

Step 1. Start with a GEP [15]. This gives the two loading matrices \mathbf{A} and \mathbf{B} . The third loading matrix, \mathbf{C} , is obtained by a least squares step. In order to solve GEP, the matrices \mathbf{X}_1^* and \mathbf{X}_2^* need to be transferred into square matrices. This can be done by using a common space [15] on to which both matrices are projected. In this paper, the common space was based on $\mathbf{X}_1^* + \mathbf{X}_2^*$.

Step 2. Recognize the triad which is constant and permute the model such that the third triad models the constant. Note that there is a permutation freedom between triads. In this case, the third column of \mathbf{A} , \mathbf{a}_3 , has to be constant and hence vector \mathbf{c}_3 , the third column of \mathbf{C} , has to be equal to $(1 \ 1)^T$. The reaction rate constants k_1 and k_2 can be estimated directly from the scaling factors listed in the first two columns of the \mathbf{C} matrix if the time shift is known (see Section 2).

Note that a GEP not always gives satisfactory results, because it can produce complex results. The third column of \mathbf{A} and \mathbf{C} are known beforehand. However, this knowledge is not used by GRAM. Hence, comparing the results of GRAM with these columns gives a check on the quality of the obtained results.

GRAM and LM-PAR

- 1) Use a generalized eigenvalue problem to decompose the three-way array $\underline{\mathbf{X}}^*$ ($(M-S) \times N \times 2$) in the three loading matrices $\mathbf{A}^{(0)}$, $\mathbf{B}^{(0)}$ and $\mathbf{C}^{(0)}$.
- 2) Estimate the reaction rate constants from the scaling factors listed in $\mathbf{C}^{(0)}$.

Extra steps in case of using LM-PAR

- 3) Define $\tilde{\mathbf{A}}^{(0)}$ and $\tilde{\mathbf{C}}^{(0)}$ (reconstruction of concentration profiles and ratio's using the estimated reaction rate constants) and $\tilde{\mathbf{B}}^{(0)}$ (least squares PARAFAC fit).
- 4) Subtract the contribution from the column with constants from the three-way array $\underline{\mathbf{X}}^*$: $\tilde{\underline{\mathbf{X}}}^{*(0)} = \underline{\mathbf{X}}^* - \mathbf{a}_3^{(0)}(\mathbf{c}_3^{(0)T} \otimes \tilde{\mathbf{b}}_3^{(0)T})$.
- 5) Matrices are partitioned:

$$\tilde{\mathbf{A}}^{(0)} = [\tilde{\mathbf{A}}^{(0)}, \mathbf{a}_3^{(0)}], \tilde{\mathbf{C}}^{(0)} = [\tilde{\mathbf{C}}^{(0)}, \begin{pmatrix} 1 \\ 1 \end{pmatrix}] \text{ and } \tilde{\mathbf{B}}^{(0)} = [\tilde{\mathbf{B}}^{(0)}, \tilde{\mathbf{b}}_3^{(0)}].$$
- 6) $\min_{k_1, k_2} \|\tilde{\underline{\mathbf{X}}}^{*(0)} - \tilde{\mathbf{A}}^{(0)}(\tilde{\mathbf{C}}^{(0)T} \otimes \tilde{\mathbf{B}}^{(0)T})\|^2$ using the Levenberg-Marquardt algorithm. Update $\tilde{\mathbf{A}}^{(0)}$ and $\tilde{\mathbf{C}}^{(0)}$ using the optimal values for k_1 and k_2 according to the Levenberg-Marquardt algorithm.
- 7) Update $\tilde{\mathbf{B}}^{(0)}$ using a least-squares PARAFAC step.
- 8) Repeat step 4 to step 7, until the convergence criterion is fulfilled.

Convergence criterion: Stop the iterations if the relative change in fit between two iterations is below 10^{-6} .

Fig. 9. Summary of the most important steps of GRAM and LM-PAR. The different vectors and matrices are explained in the text.

2.3.2. Iterative algorithm: the Levenberg–Marquardt algorithm and alternating least squares steps of the PARAFAC model (LM–PAR)

LM–PAR, which is monotonically decreasing, will be explained in this section. For all the estimations obtained with LM–PAR in this paper, the GRAM results were used as initial values.

Steps 1 and 2 of LM–PAR are equal to GRAM. Let the three matrices \mathbf{A} , \mathbf{B} and \mathbf{C} obtained from the first step of GRAM be $\mathbf{A}^{(0)}$, $\mathbf{B}^{(0)}$ and $\mathbf{C}^{(0)}$, respectively. Let

the estimated k_1 and k_2 obtained by the second step of GRAM be $\text{start-}k_1$ and $\text{start-}k_2$, respectively. The superscript zero indicates that no iterations have occurred yet.

Step 3. The $\mathbf{C}^{(0)}$ matrix from the first step of GRAM has the following form:

$$\mathbf{C}^{(0)} = \begin{pmatrix} u & v & 1 \\ x & y & 1 \end{pmatrix}.$$

Define $\tilde{\mathbf{C}}^{(0)}$ according to the following equation:

$$\tilde{\mathbf{C}}^{(0)} = \begin{pmatrix} 1 & 1 & 1 \\ d_1 & d_2 & 1 \end{pmatrix}, \quad (14)$$

where $d_1 = x/u$ and $d_2 = y/v$. Because the $\mathbf{C}^{(0)}$ matrix has been transformed into $\tilde{\mathbf{C}}^{(0)}$, a transformed matrix $\tilde{\mathbf{B}}^{(0)}$ has to be constructed too. This is done by a three-way least squares fit (PARAFAC fit) from the three-way array $\underline{\mathbf{X}}^*$, $\tilde{\mathbf{C}}^{(0)}$ and $\tilde{\mathbf{A}}^{(0)}$, where $\tilde{\mathbf{A}}^{(0)}$ is a matrix with the reconstructed exponentially decaying functions using start- k_1 and start- k_2 for k_1 and k_2 , respectively, according to the following equation:

$$\tilde{\mathbf{A}}^{(0)} = [\tilde{\mathbf{A}}^{(0)}, \tilde{\mathbf{a}}_3^{(0)}] = [\tilde{\mathbf{a}}_1^{(0)}, \tilde{\mathbf{a}}_2^{(0)}, \tilde{\mathbf{a}}_3^{(0)}], \quad (15)$$

where $\tilde{\mathbf{a}}_1^{(0)} = h \cdot e^{-k_1 t}$, $\tilde{\mathbf{a}}_2^{(0)} = h \cdot e^{-k_2 t}$, and h is a fixed constant. The vector $(e^{-k_1 t_1} \dots e^{-k_1 t_{(M-S)}})^T$ is reduced to the shorthand notation $e^{-k_1 t}$ and $\mathbf{t} = (t_1 \dots t_{(M-S)})^T$. The third column of $\tilde{\mathbf{A}}^{(0)}$ remains the column with constants, $\mathbf{a}_3^{(0)}$.

Step 4. Define $\tilde{\mathbf{X}}^{*(0)}$ according to the following equation in order to correct for the contribution of the column with constants:

$$\tilde{\mathbf{X}}^{*(0)} = \underline{\mathbf{X}}^* - \mathbf{a}_3^{(0)} (\mathbf{c}_3^{(0)T} \otimes \tilde{\mathbf{b}}_3^{(0)T}), \quad (16)$$

where \otimes denotes the Kronecker product.

Step 5. Next, matrices are partitioned:

$$\tilde{\mathbf{C}}^{(0)} = \begin{pmatrix} 1 & 1 \\ d_1 & d_2 \end{pmatrix}, \quad \tilde{\mathbf{C}}^{(0)} = \left[\tilde{\mathbf{C}}^{(0)}, \begin{pmatrix} 1 \\ 1 \end{pmatrix} \right],$$

$$\tilde{\mathbf{A}}^{(0)} = [\tilde{\mathbf{a}}_1^{(0)}, \tilde{\mathbf{a}}_2^{(0)}], \quad \tilde{\mathbf{A}}^{(0)} = [\tilde{\mathbf{A}}^{(0)}, \mathbf{a}_3^{(0)}],$$

$$\tilde{\mathbf{B}}^{(0)} = [\tilde{\mathbf{B}}^{(0)}, \tilde{\mathbf{b}}_3^{(0)}].$$

The loading matrices with a single tilde consist of three columns and the matrices with a double tilde consist of two columns. Both $\tilde{\mathbf{a}}_1^{(0)}$ and $\tilde{\mathbf{a}}_2^{(0)}$ are a function of d_1 and d_2 , respectively, and hence, these are a function of k_1 , k_2 and S .

Step 6. The following equation is minimized over k_1 and k_2 ensuring that for the proper k_1 and k_2 this minimum will be attained:

$$\min_{k_1, k_2} \|\tilde{\mathbf{X}}^{*(0)} - \tilde{\mathbf{A}}^{(0)} (\mathbf{C}^{(0)T} \otimes \mathbf{B}^{(0)T})\|^2, \quad (17)$$

where $\tilde{\mathbf{B}}^{(0)}$ and $\tilde{\mathbf{X}}^{*(0)}$ are kept constant and $\tilde{\mathbf{A}}^{(0)}$ and $\mathbf{C}^{(0)}$ are both a function of k_1 and k_2 . During the optimization procedure k_1 and k_2 are updated using the Levenberg–Marquardt algorithm [27]. This algo-

rithm, for finding an optimum in a response surface, smoothly varies between two methods for finding the optimum, the steepest decent method, that is used *far* from the optimum, and the inverse Hessian method, that is used *close* to the optimum. For every update of k_1 and k_2 , an update for $\tilde{\mathbf{A}}^{(0)}$ according to Eq. (15) and an update for $\tilde{\mathbf{C}}^{(0)}$ according to the following equation will be performed, simultaneously:

$$\tilde{\mathbf{C}}^{(0)} = \begin{pmatrix} 1 & 1 \\ d_1 & d_2 \end{pmatrix}, \quad (18)$$

where $d_1 = 1/e^{k_1 S}$, $d_2 = 1/e^{k_2 S}$ and S is the time shift.

Step 7. The Levenberg–Marquardt algorithm gives least squares $\tilde{\mathbf{A}}^{(0)}$ and $\tilde{\mathbf{C}}^{(0)}$. These matrices will be called $\tilde{\mathbf{A}}^{(1)}$ and $\tilde{\mathbf{C}}^{(1)}$, respectively. Hence every set of Levenberg–Marquardt iterations to obtain optimal values for k_1 and k_2 is called *one* iteration, indicated by the superscript “(1)”. The following matrices can be constructed:

$$\tilde{\mathbf{A}}^{(1)} = [\tilde{\mathbf{A}}^{(1)}, \mathbf{a}_3^{(0)}] \quad \text{and} \quad \tilde{\mathbf{C}}^{(1)} = \left[\mathbf{C}^{(1)}, \begin{pmatrix} 1 \\ 1 \end{pmatrix} \right].$$

Update $\tilde{\mathbf{B}}^{(0)}$ to $\tilde{\mathbf{B}}^{(1)}$ with $\tilde{\mathbf{A}}^{(1)}$, $\tilde{\mathbf{C}}^{(1)}$ and $\tilde{\mathbf{X}}^*$ by means of a least squares PARAFAC fit.

Step 8. Repeat steps 4–7 until the convergence criterion is fulfilled. In this paper the following convergence criterion has been used. Calculate the loss function according to the following equation after each iteration.

$$f(i) = \text{SSQ}(\tilde{\mathbf{X}}^{*(i)} - \tilde{\mathbf{A}}^{(i)} \mathbf{C}^{(i)T} \otimes \tilde{\mathbf{B}}^{(i)T}), \quad (19)$$

where SSQ is the sum of squares. If the following equation holds, the iterations are stopped:

$$\frac{f^{(i-1)} - f^{(i)}}{f^{(i)}} < 10^{-6}. \quad (20)$$

2.4. Quality assessment of the estimated reaction rate constants

If the reaction rate constants are estimated, there will be a certain fluctuation between the several estimated parameters. This can be caused by model errors, experimental errors and instrumental noise. The model errors can be kept very small if the correct kinetic model is used and the law of Lambert–Beer is

valid. Experimental errors are always present and are caused by concentration errors and errors due to the start of the reaction, for example. Instrumental noise is also always present and is caused by variations of the instrument. If reaction rate constants are estimated for several repeated individual batch processes and the individual standard deviation is estimated, this represents the upper error limit. Note that this is the worst case, because both experimental errors and instrumental noise are involved.

A lower error limit caused by mainly instrumental noise is estimated using the jackknife method. The theory of the jackknife method is very well explained in the book by Shao and Tu [21]. Consider the mean batch run obtained from averaging all the repeated individual batch process runs. Hence, experimental errors and also instrumental noise are averaged. In the jackknife procedure a fixed number of spectra from the three-way array $\tilde{\mathbf{X}}^*$ based on the mean batch run are left out several times according to a fixed interval, and hence the three-way array $\tilde{\mathbf{X}}^*$ is reduced. Finally, for the mean batch process a set of estimations for the reaction rate constants are obtained. The individual standard deviation of these estimations represents the lower error limit, because mainly instrumental noise is involved. The jackknife procedure is visualized in Fig. 10, where a two-way representation of the three-way array by means of unfolding $\tilde{\mathbf{X}}^*$ is given to illustrate the jackknife procedure much easier.

Assume that the jackknife interval equals 4 and $(M-S)$ equals 20. In the first step the rows 1, 5, 9, 13 and 17 are removed and the kinetic parameters are estimated

using the remaining 15 rows of the two-way representation. In the second step the rows 2, 6, 10, 14 and 18 are removed and the kinetic parameters are again estimated on the basis of the other 15 rows, etc.

3. Simulations: set-up

For the simulations, the first-order consecutive reaction, already described in Section 2 of this paper, was used as kinetic model system. Pure SW-NIR spectra were simulated for the three individual species for the wavelength range 850–1050 nm with increments of 1 nm using Gaussian peaks. The time range was chosen from 0 to 20 min with increments of 1 min. The peak maxima of the species U , V and W corresponded to different wavelengths to control the amount of spectral overlap. A small overlap corresponded to a peak maximum of 900, 950 and 1000 nm for the species U , V and W , respectively. A strong spectral overlap corresponded to a peak maximum of 930, 950 and 970 nm for the species U , V and W , respectively. The pure spectra of the individual species with a small and a strong spectral overlap are shown in Fig. 11. White Gaussian distributed noise was added to the spectra with a sigma defined as a percentage of the maximum absorbance of the simulated SW-NIR spectrum at time 0. For every situation 100 SW-NIR datasets were simulated. Details about the set-up of the simulated data can be found in an earlier paper [8].

The simulations were performed with GRAM and LM-PAR under different simulated conditions: different amounts of peak overlap and different noise levels. The used values for the reaction rate constants were always 0.30 and 0.05 min⁻¹ for k_1 and k_2 , respectively. The time shift parameter S was equal to 1 and the values of the elements in the column with constants were equal to 100 000.

4. Experimental

4.1. The reaction

The following two-step epoxidation of 2,5-di-*tert*-butyl-1,4-benzoquinone [5,8,20] using *tert*-butyl hydroperoxide and Triton B catalyst was used as a

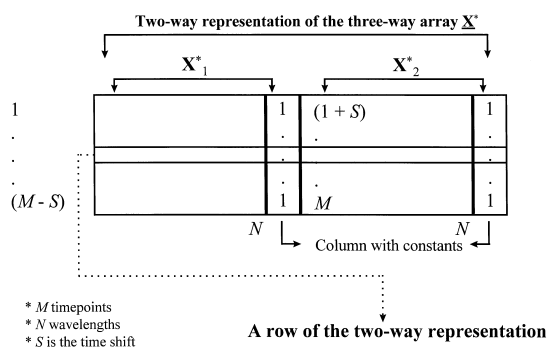


Fig. 10. Visualization of the jackknife method by unfolding the three-way array \mathbf{X}^* into the matrices \mathbf{X}_1^* and \mathbf{X}_2^* .

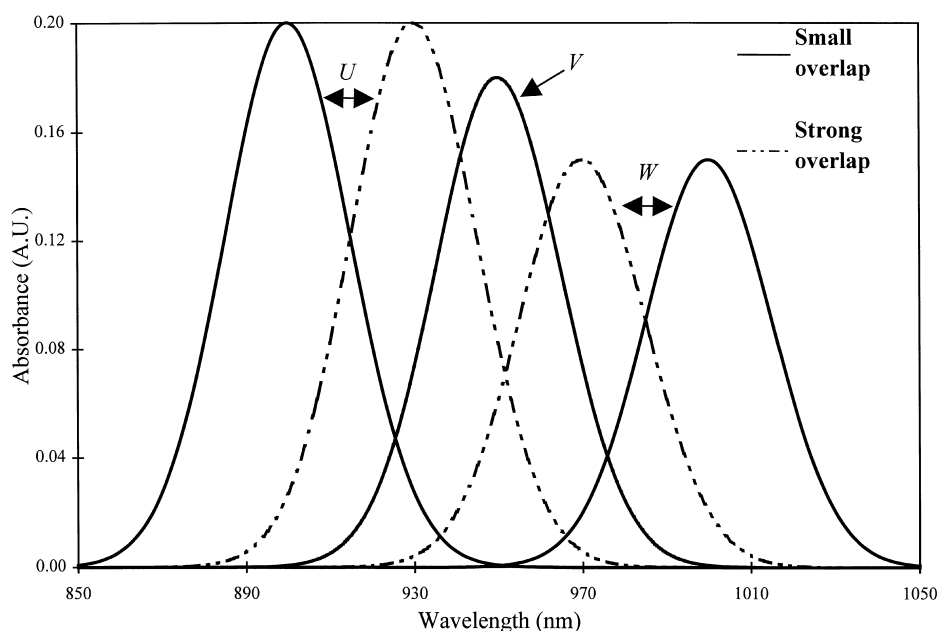
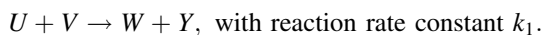


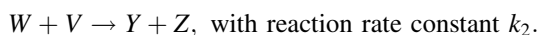
Fig. 11. The pure spectra of the individual species *U*, *V* and *W* for the SW-NIR simulations. The peak of species *V* is the same for the small and strong overlap.

real experimental example process.

Step 1 :



Step 2 :



The species *U*, *V*, *W*, *Y* and *Z* are specified in Table 1.

If the *tert*-butyl hydroperoxide is present in large excess, pseudo-first-order kinetics can be observed and the kinetic Eqs. (5)–(7) can be used to describe the concentration profiles of the spectroscopic active species *U*, *W* and *Z*, respectively. These three species (reactant, intermediary and product) will be monitored

in this paper. The reagents, sample preparation and experimental set-up have been described extensively in an earlier paper [8]. A spectrophotometer with diode array detection was used to measure SW-NIR spectra of the reacting system. A quartz cuvette (Hellma Benelux) with 10.00 cm pathlength was used to obtain spectra of the reaction mixture. A Pt-100, a constant temperature bath (Neslab) and an immersion cooler (Haake) were used to control the temperature inside the cuvette. The most important experimental conditions are given in Table 2.

Table 1

The different species involved in the two-step epoxidation of 2,5-di-*tert*-butyl-1,4-benzoquinone

<i>U</i>	2,5-di- <i>tert</i> -butyl-1,4-benzoquinone
<i>V</i>	<i>tert</i> -butyl hydroperoxide
<i>W</i>	2,5-di- <i>tert</i> -butyl mono-epoxide-1,4-benzoquinone
<i>Y</i>	<i>tert</i> -butyl alcohol
<i>Z</i>	<i>cis</i> and <i>trans</i> 2,5-di- <i>tert</i> -butyl di-epoxide-1,4-benzoquinone

Table 2

Experimental conditions

Reaction temperature	17°C
Integration time ^a	1 s
Sampling time	5 s
Total run time	1200 s
Wavelength range	800–1100 nm
Wavelength interval	1.0 nm
Number of recorded spectra	240

^aIt took 1 s to measure 10 spectra from 800 to 1100 nm. These spectra were averaged.

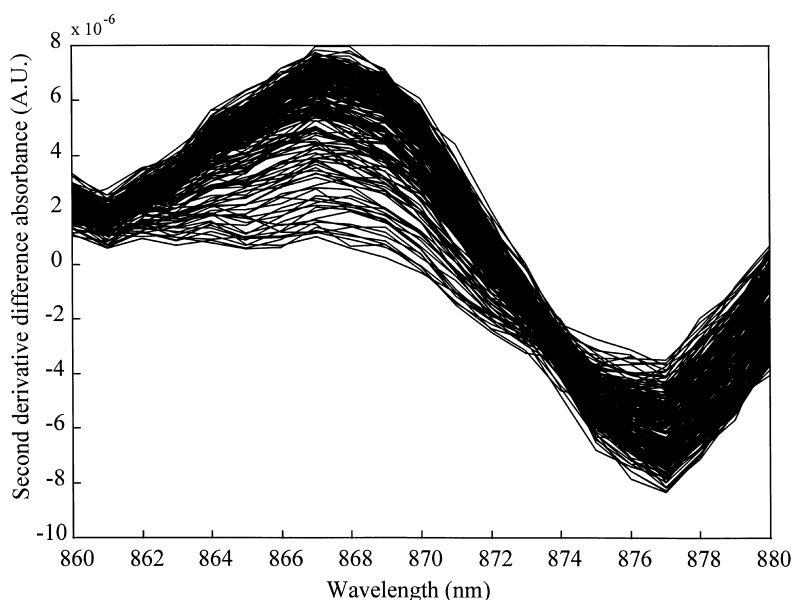


Fig. 12. The second derivative difference spectra for the wavelength range 860–880 nm of one individual batch process.

4.2. Data processing

The data processing procedure is described in an earlier paper [8]. Here a short summary of the most important aspects is given. The spectra of one individual batch process run are shown in a previous paper [8]. The first few spectra do not match with the other spectra, because these spectra are the first just after addition of the catalyst and it takes some time to mix very well. The reproducibility of each recorded spectrum was calculated in order to decide which spectra had to be deleted and which spectrum had to be used as blank in order to estimate second derivative difference spectra. Based on this criterion, the fourth spectrum was used as blank. A Savitzky–Golay filter [28] of 15 data points was used to estimate the second derivative spectra in order to remove baseline effects and drift. To stress the spectral features from the appearing and disappearing species, second derivative difference spectra were calculated by subtracting the blank from all the other spectra. This is necessary because the main spectral features are caused by the solvents and the catalyst. The second derivative difference spectra of one individual batch process are shown in Fig. 12.

The second derivative difference spectra were used to apply GRAM and LM–PAR as described in Sec-

tion 2. A limited wavelength range of the second derivative difference spectra was used for data processing because of the increasing absorbance of the by-product *tert*-butyl alcohol, formed during the reaction, and the decreasing absorbance of *tert*-butylhydroperoxide. If the wavelength range 860–880 nm is considered, the spectral features are caused by the three benzoquinone species [5]. The values of the elements in the column with constants were equal to 1.

Data processing was performed in the Matlab environment (Version 4.2C, The Mathworks) on a Pentium 133 MHz Personal Computer with 64 MB RAM and a 1.2 GB hard disk.

5. Results and discussion

5.1. Simulations

The mean values for both k_1 and k_2 estimations with GRAM and LM–PAR are listed in Table 3 for two different noise levels (1% and 4%) and four different situations of peakoverlap of the individual spectrum of the species. From the estimations of the reaction rate constants obtained from GRAM and LM–PAR the following aspects can be observed.

Table 3

Mean estimated k_1 and k_2 values with individual standard deviations (STDs) for 100 simulated sets of SW-NIR spectra for two different noise levels and four different situations of peak overlap

$P_{\max,A}$ (nm)	$P_{\max,B}$ (nm)	$P_{\max,C}$ (nm)	Noise level (%)	Mean k_1 (min ⁻¹)	Mean k_2 (min ⁻¹)	STD k_1 (min ⁻¹)	STD k_2 (min ⁻¹)
900	950	1000	1	0.2995 (0.2996)	0.0503 (0.0503)	0.0030 (0.0024)	0.0029 (0.0026)
			4	0.2989 (0.2995)	0.0494 (0.0490)	0.0106 (0.0097)	0.0117 (0.0108)
910	950	990	1	0.2998 (0.2996)	0.0504 (0.0504)	0.0030 (0.0023)	0.0030 (0.0028)
			4	0.2946 (0.2951)	0.0528 (0.0519)	0.0122 (0.0096)	0.0124 (0.0111)
920	950	980	1	0.2996 (0.2997)	0.0501 (0.0501)	0.0030 (0.0025)	0.0032 (0.0030)
			4	0.2937 (0.2948)	0.0523 (0.0514)	0.0129 (0.0107)	0.0129 (0.0116)
930	950	970	1	0.2993 (0.2996)	0.0501 (0.0500)	0.0042 (0.0034)	0.0039 (0.0036)
			4	0.2903 (0.2941)	0.0505 (0.0496)	0.0166 (0.0130)	0.0157 (0.0142)

$P_{\max,i}$ indicates the spectral position of the peak maximum of species i . The values were obtained with GRAM and the values between parentheses were obtained with LM-PAR for the same simulated datasets. The true values were 0.30 and 0.05 min⁻¹ for k_1 and k_2 , respectively.

1. A higher noise level results in a larger standard deviation for both k_1 and k_2 estimations.
2. If the noise level is kept constant and the spectral overlap becomes stronger, the standard deviations for k_1 and k_2 become larger.
3. If LM-PAR is used instead of GRAM, the standard deviation is smaller for both kinetic parameters and the mean estimated values are closer to the real values.

If the noise level is increased to higher values than 4%, many estimated k_1 values will be equal to the estimated k_2 values. This is illustrated with the following simulations. For a fixed peak overlap ($P_{\max,A}=900$ nm, $P_{\max,B}=950$ nm and $P_{\max,C}=1000$ nm) 100 SW-NIR datasets were simulated for two different noise levels (10% and 15%). The kinetic parameters were estimated with GRAM. For a noise level of 10% in five cases k_1 equals k_2 . For a noise level of 15% in 27 cases k_1 equals k_2 . A possible explanation for this phenomenon is that if the noise level is very high, it is very hard to distinguish between the two exponential functions $e^{-k_1 t}$ and $e^{-k_2 t}$. If this noise effect occurs, this can easily be detected from the C

matrix, because the first two columns will be equal and hence k_1 equals k_2 .

The choice of the column with constants appeared to be very important. If the constants are equal to 1 the third column of **A** and **C** is not always constant. If the column with constants is much larger than “the signal”, **a**₃ and **c**₃ are forced to be constant.

5.2. Experiments

5.2.1. Effect of the time shift on the reaction rate constant estimations

It is very hard to decide, in advance, how large the time shift parameter has to be. If the time shift is very small, the two formed datasets from the master dataset are nearly the same. If the time shift is very large, the two formed datasets will become too small and this will result in very bad estimations of the kinetic parameters. Hence, for every specific problem the optimal choice of the time shift parameter has to be determined. In order to investigate the effect of different time shifts, the kinetic parameters were estimated for eight repeated individual batch processes with GRAM for different time shifts. The results are

Table 4

The mean estimated reaction rate constants and the individual standard deviations (STDs) for eight repeated individual batch processes

Time shift	Mean k_1 (min^{-1})	Mean k_2 (min^{-1})	STD k_1 (min^{-1})	STD k_2 (min^{-1})
10 (5)	0.25	0.09	0.05	0.04
20 (7)	0.28	0.10	0.02	0.07
30 (8)	0.28	0.10	0.03	0.06
40 (7)	0.26	0.10	0.02	0.05
50 (7)	0.25	0.11	0.02	0.05
60 (6)	0.24	0.09	0.02	0.03
70 (4)	0.27	0.07	0.03	0.02
80 (4)	0.26	0.09	0.04	0.05
90 (6)	0.29	0.12	0.08	0.02
100 (5)	0.31	0.14	0.10	0.05

The values were obtained for different time shifts. GRAM was used. The values between brackets from the column with the time shifts indicate how many estimations result in $k_1 \neq k_2$ and $k_2 > 0$. Hence, (5) indicates that three repeated individual batch processes result in $k_1 = k_2$ or $k_2 < 0$. These values are left out and hence the mean values are calculated over five estimations.

listed in Table 4. From this table the following aspects can be observed.

1. A small or a large time shift results in k_1 estimations which are equal to k_2 . The phenomenon was also present in the simulations if the noise level was increased. Probably, it is very hard to distinguish between the two exponentially decaying functions if the noise level is very high

or the time shift parameter is too large or too small.

2. A small or a large time shift can result in k_2 estimations which are negative. Negative reaction rate constants are physically meaningless.
3. A time shift of roughly 30 or 40 datapoints gives the best results. This gives the lowest standard deviation for k_1 and a compromise in standard deviation for k_2 .

A time shift of 30 datapoints is the only situation where for all eight repeated individual batch processes $k_1 \neq k_2$ and $k_2 > 0$ and therefore the estimations can be compared to those of an earlier paper [8]. For these reasons a time shift of 30 datapoints will be used in the remainder of this section.

5.2.2. Estimation of the upper error limit

The individual estimations of the kinetic parameters for each repeated individual batch process and the mean batch process are listed in Table 5 for a time shift of 30 datapoints. The mean batch process was obtained by averaging the eight repeated individual batch processes. GRAM and LM-PAR were both used. The individual standard deviations represent the upper error limit. This is the worst case, because both experimental errors and instrumental noise are involved. Hence, there is no averaging effect. From Table 5 the following aspects can be observed.

Table 5

The individual estimated reaction rate constants for eight repeated individual batch processes and the mean batch process

Number batch run	Estimated k_1 (min^{-1})	Estimated k_2 (min^{-1})
1	0.2779 (0.2521)	0.1097 (0.1044)
2	0.3268 (0.2899)	0.0804 (0.0773)
3	0.2756 (0.2757)	0.0775 (0.0774)
4	0.2934 (0.1881)	0.1721 (0.1232)
5	0.2643 (0.2345)	0.1358 (0.1229)
6	0.2865 (0.2734)	0.0132 (0.0132)
7	0.2818 (0.2787)	0.0578 (0.0571)
8	0.2197 (0.1841)	0.1752 (0.1489)
Mean batch process	$\bar{k}_1 = 0.28$, STD = 0.03 ($\bar{k}_1 = 0.25$, STD = 0.04) 0.2756 (0.2677)	$\bar{k}_2 = 0.10$, STD = 0.06 ($\bar{k}_2 = 0.09$, STD = 0.04) 0.0668 (0.0666)

A time shift of 30 datapoints was used. The values were obtained with GRAM. The values between parentheses were obtained with LM-PAR. The mean values (\bar{k}_1 and \bar{k}_2) and the individual standard deviations (STDs) based on the eight individual estimated kinetic parameters from batch number 1–8 are also given.

1. If the individual standard deviations are considered, the standard deviation is smaller for k_2 if LM-PAR is used instead of GRAM.
2. The spread of the k_2 estimations is larger than the spread of the k_1 estimations because k_1 is more dominant than k_2 . A large spread in general is caused by the high noise level of the experimental data.
3. GRAM estimates nearly always higher values for the kinetic parameters than LM-PAR.

There appeared to be a big difference in speed between GRAM and LM-PAR. In this case GRAM only took a few seconds whereas LM-PAR took a few hours.

5.2.3. Estimation of the lower error limit

The jackknife procedure described in Section 2 was used to estimate the lower error limit. The jackknife interval was chosen equal to 26. Finally this resulted in ten jackknife estimations for k_1 and k_2 for the mean batch process. The jackknife procedure was applied for both algorithms. The time shift was again equal to 30 datapoints. The mean estimated kinetic parameters based on ten jackknife estimations and the corresponding individual standard deviations (lower error limits) obtained with both algorithms are listed in Table 6. The lower error limit represents mainly instrumental noise. From Table 6 it is observed that the use of LM-PAR leads to a decrease of the influence of instrumental error for the k_1 estimations.

5.3. Summary results

LM-PAR performs better than GRAM. Simulations and experimental data showed that both algorithms can deal with high spectral overlap. From experimen-

tal data, the optimal time shift appears to be roughly 30 or 40 datapoints. Experimental data showed that if the time shift is small or large, k_1 and k_2 estimations can be equal. Simulations showed that these estimations can also be equal if the noise level is increased. This is a noise problem, because probably no distinction can be made between the two exponentially decaying functions. This problem can easily be detected, because if k_1 equals k_2 the first two columns of the C-matrix will be the same. If the upper limit is considered and the performance of LM-PAR is compared to the performance of GRAM, the standard deviation is smaller for the k_2 estimations if LM-PAR is used. GRAM estimations are always higher than LM-PAR estimations. For the lower error limit the standard deviation is approximately a factor two small for the k_1 estimations using LM-PAR instead of GRAM. Despite the fact that the standard deviations for the estimated kinetic parameters are smaller if LM-PAR is used instead of GRAM, the last mentioned method is very powerful if rapid estimations of reaction rate constants are necessary.

6. Conclusion

In this paper GRAM has been used in order to estimate reaction rate constants from on-line SW-NIR measurements of a reacting system. The interpretation is very easy. The third factor of the three-way array, C, gives the reaction rate constants. LM-PAR can be used if accurate estimations of the reaction rate constants are desirable. GRAM can be used to obtain rough estimations of reaction rate constants very fast. Simulations showed that both algorithms can deal with a strong spectral overlap. If the noise level is increased, the estimated values of the reaction rate constants can become equal for a simulated dataset. From the

Table 6
The results from the jackknife procedure of the mean batch process

Mean k_1 (min^{-1})	Mean k_2 (min^{-1})	STD k_1 (min^{-1})	STD k_2 (min^{-1})
0.28 (0.27)	0.07 (0.07)	2.00×10^{-3} (1.10×10^{-3})	1.60×10^{-3} (1.50×10^{-3})

The mean kinetic parameters are the mean over 10 jackknife estimations. The standard deviations (STDs) represent the lower error limit. A time shift of 30 datapoints was used. The values were obtained with GRAM. The values between parentheses were obtained with LM-PAR.

simulations it can be concluded that LM-PAR always leads to more precise estimations for the reaction rate constants compared to GRAM.

The two-step epoxidation of 2,5-di-*tert*-butyl-1,4-benzoquinone showed a small difference between GRAM and LM-PAR, but LM-PAR always leads to more precise estimations for the reaction rate constants compared to GRAM. The optimal time shift appeared to be roughly 30 or 40 datapoints in this case.

If the time shift parameter is too large or too small, the estimations of the reaction rate constants can become equal. Probably, it is very hard to distinguish between exponentially decaying functions for these choices of the time shift parameter. Upper and lower error limits were also estimated for quality assessment.

GRAM is a very powerful method for estimating reaction rate constants very fast. The speed of the algorithm is known in advance, because it is non-

Table 7
Nomenclature

Variable	Description
\mathbf{A} $((M-S) \times 3)$	The matrix with concentration profiles obtained from a GEP
$\mathbf{A}^{(j)}$ $((M-S) \times 3)$	The matrix \mathbf{A} after the j th iteration
$\tilde{\mathbf{A}}$ $((M-S) \times 3)$	The new matrix \mathbf{A} obtained by an initial estimate for k_1 and k_2
$\tilde{\mathbf{A}}$ $((M-S) \times 2)$	The first two columns of matrix $\tilde{\mathbf{A}}$
\mathbf{a}_i	The i th column of matrix \mathbf{A}
$\mathbf{a}_i^{(j)}$	The i th column of matrix \mathbf{A} after the j th iteration
\mathbf{B} $((N+1) \times 3)$	The matrix with combined spectra obtained from a GEP
\mathbf{C} (2×3)	The matrix with scaling factors obtained from a GEP
$C_{U,0}$	The initial concentration of species U
$C_{U,i}$	The concentration of species U at time point i ; $C_{V,i}$ and $C_{W,i}$ for V and W , respectively
\mathbf{D} $(N \times K)$	Matrix with pure spectra
\mathbf{d}_U $(N \times 1)$	Pure spectrum of species U ; \mathbf{d}_V and \mathbf{d}_W for V and W , respectively
\mathbf{E} $(M \times N)$	Matrix with errors
$\underline{\mathbf{E}}$ $((M-S) \times N \times 2)$	Three-way matrix with errors
\mathbf{E}^* $((M-S) \times (N+1) \times 2)$	Three-way matrix with errors
\mathbf{F} $(M \times K)$	Matrix with concentration profiles
\mathbf{f}_U $(M \times 1)$	Concentration profile of species U ; \mathbf{f}_V and \mathbf{f}_W for V and W , respectively
\mathbf{f}_L $(M \times 1)$	The concentration profile of the added column with constants
\mathbf{f}_1	The concentration profile of matrix \mathbf{X}_1
\mathbf{f}_2	The concentration profile of matrix \mathbf{X}_2
$f^{(i)}$	Loss function after the i th iteration
h	A fixed constant
k_1, k_2	Reaction rate constants
k	Equals $k_1/(k_2-k_1)$
\bar{k}_1, \bar{k}_2	Mean estimated k_1 and k_2
\mathbf{s}_U $((N+1) \times 1)$	Pure spectrum of species U ; \mathbf{s}_V and \mathbf{s}_W for V and W , respectively
\mathbf{s}_L $((N+1) \times 1)$	The pure spectrum of the added column with constants
S	The time shift parameter
\mathbf{t}	Time vector with dimension $(M \times 1)$ or $((M-S) \times 1)$
T (superscript)	Transpose of a matrix or vector
t_i	The time at point i
\mathbf{X} $(M \times N)$	Matrix with spectra during a certain time course
\mathbf{X}_1 $((M-S) \times N)$	Datamatrix 1 formed by splitting \mathbf{X}
\mathbf{X}_2 $((M-S) \times N)$	Datamatrix 2 formed by splitting \mathbf{X}
\mathbf{X}^* $(M \times (N+1))$	The augmented datamatrix
\mathbf{X}_1^* $((M-S) \times (N+1))$	Datamatrix 1 formed by splitting \mathbf{X}^*
\mathbf{X}_2^* $((M-S) \times (N+1))$	Datamatrix 2 formed by splitting \mathbf{X}^*
$\underline{\mathbf{X}}^*$ $((M-S) \times (N+1) \times 2)$	The three-way array formed by stacking \mathbf{X}_1^* and \mathbf{X}_2^*
$\underline{\mathbf{X}}$ $((M-S) \times N \times 2)$	The three-way array formed by stacking \mathbf{X}_1 and \mathbf{X}_2

Table 8
Dimensional descriptors

Variable	Description
<i>K</i>	The number of species
<i>M</i>	The number of time points
<i>N</i>	The number of wavelengths
<i>P</i>	The number of stacked matrices
<i>R</i>	The three-way rank

iterative. GRAM can be used if a rough estimation of the kinetic parameters is desirable, for instance if (batch) processes are to be monitored. LM-PAR is in this case not very convenient to use because of the time consuming iterations. In the case of LM-PAR the speed of the algorithm is not known in advance. If the batch time is elapsed, LM-PAR can be used to estimate accurately kinetic parameters. Since many measurements are based on exponentially decaying functions, GRAM and LM-PAR can have many applications.

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Appendix A

Nomenclature

In general, boldface capital characters denote matrices and boldface lower case characters denote vectors. Tables 7 and 8 summarize the nomenclature of some important scalars, vectors and matrices used in this paper.

References

- [1] S.D. Brown, *Anal. Chem.* 62 (1990) 84R.
- [2] J.J. Workman Jr., *Appl. Spectrosc. Rev.* 31 (1996) 251.
- [3] W.H. Lawton, E.A. Sylvestre, *Technometrics* 13 (1971) 617.
- [4] E.A. Sylvestre, W.H. Lawton, M.S. Maggio, *Technometrics* 16 (1974) 353.
- [5] D.M. Mayes, J.J. Kelly, J.B. Callis, in: K.I. Hildrum, T. Isaksson, T. Naes, A. Tandberg (Eds.), *Near Infra-Red Spectroscopy: Bridging the Gap between Data Analysis and NIR Applications*, Ellis Horwood, Chichester, 1992, pp. 377–387.
- [6] K.Y. Tam, F.T. Chau, *Chemometrics Intell. Lab. Syst.* 25 (1994) 25.
- [7] J.L. González, M.M. Canedo, C. Grande, *Chemometrics Intell. Lab. Syst.* 39 (1997) 77.
- [8] S. Bijlsma, D.J. Louwerse (Ad), A.K. Smilde, *AIChE Journal* 1997, accepted.
- [9] R.I. Shrager, R.W. Hendler, *Anal. Chem.* 54 (1982) 1147.
- [10] S.D. Frans, J.M. Harris, *Anal. Chem.* 56 (1984) 466.
- [11] S.D. Frans, J.M. Harris, *Anal. Chem.* 57 (1985) 1718.
- [12] R.I. Shrager, *Chemometrics Intell. Lab. Syst.* 1 (1986) 59.
- [13] B. Antalek, W. Windig, *J. Am. Chem. Soc.* 118 (1996) 10331.
- [14] W. Windig, B. Antalek, *Chemometrics Intell. Lab. Syst.* 37 (1997) 241.
- [15] E. Sanchez, B.R. Kowalski, *Anal. Chem.* 58 (1986) 496.
- [16] B. Wilson, E. Sanchez, B.R. Kowalski, *J. Chemometrics* 3 (1989) 493.
- [17] R.A. Harshman, *UCLA Working Pap. Phonet.* 16 (1970) 1.
- [18] A.K. Smilde, *Chemometrics Intell. Lab. Syst.* 15 (1992) 143.
- [19] R.A. Harshman, M.E. Lundy, *Comput. Stat. Data Anal.* 18 (1994) 39.
- [20] E.M. Hairfield, E.W. Moomaw, R.A. Tamburri, R.A. Vigil, *J. Chem. Education* 62 (1985) 175.
- [21] J. Shao, D. Tu, *The Jackknife and Bootstrap*, Springer, New York, 1995.
- [22] D.A. Burns, E.W. Ciurczak, *Handbook of Near-Infrared Analysis*, Dekker, New York, 1992.
- [23] W. Windig, J.P. Hornak, B. Antalek, *JMR* 132 (1998) 298.
- [24] B. Antalek, J.P. Hornak, W. Windig, *JMR* 132 (1998) 307.
- [25] J.B. Kruskal, in: R. Coppi, S. Bolasco (Eds.), *Multiway Data Analysis*, Elsevier, Amsterdam, 1989, pp. 7–18.
- [26] J.B. Kruskal, R.A. Harshman, M.E. Lundy, in: R. Coppi, S. Bolasco (Eds.), *Multiway Data Analysis*, Elsevier, Amsterdam, 1989, pp. 115–122.
- [27] G.A.F. Seber, C.J. Wild, *Nonlinear Regression*, Wiley, New York, 1989.
- [28] A. Savitzky, M.J.E. Golay, *Anal. Chem.* 36 (1964) 1627.